

## A Comparative Study on the Formability Prediction of two-layer metallic Sheets

H. Deilami Azodi\* and R. Darabi

Department of Mechanical Engineering, Arak University of Technology, P.O.Box 38135-1177, Arak, Iran

**Abstract:** Two-layer metallic sheets have wide applications in aerospace, marine, automotive and domestic industries due to their superlative characteristics. In this paper, the formability of two-layer sheet is investigated through analytical, experimental and numerical approaches. An analytical model is developed based on Marciniak-Kuczynski method associated Hill's non-quadratic yield criterion. Forming limit diagrams are also obtained numerically based on finite element method using Bifurcation theory and ductile fracture criteria. Furthermore, experiments are carried out on Al3105-St14 two-layer sheet. Theoretical results from various methods are compared with results obtained from experiments to evaluate the competency of discussed analytical and numerical methods to predict the formability of two-layer sheets. The results show that analytical and numerical approaches discussed in this paper have good capabilities to predict the formability of two-layer sheets. However, the analytical method based on M-K model and numerical approach based on bifurcation theory are more suitable to determine the forming limit diagram of Al3105-St14 two-layer sheets.

**Keywords:** Forming Limit Diagram (FLD), Two-layer Sheet, Marciniak-Kuczynski (M-K) Method, Hill's Non-quadratic Yield Criterion, Bifurcation Theory, Ductile Fracture.

### 1. Introduction

As a considerable light-weight and high-strength material, two-layer sheets have generated an increasing attention. Two-layer sheets are gaining a wide array of applications due to the advantageous features in comparison with layers which compose them. Formability of sheet metal is constrained by plastic instability and localized necking. Forming limit diagram (FLD) is a commonly used tool to evaluate the formability of sheets. Initially, the definition of forming limit diagram (FLD) was presented by Keeler [1] and Goodwin [2].

Semiatin and Piehler [3, 4] investigated the formability of stainless steel-clad aluminum and aluminum-clad stainless steel sheets based on diffuse and localized necking. They concluded that arrangement of layers is the main factor in localization and fracture. Mori and Kurimoto [5] utilized deep drawing process with a cylindrical punch and stretch forming test with a hemispherical punch to investigate the formability of stainless steel-aluminum clad sheet, experimentally. They concluded that a higher formability can be achieved when the aluminum is set on the outer side of the cup in stretching and deep drawing tests. Yoshida and Hino [6] determined the forming limits of sheet metal laminates under biaxial stress conditions in 1997. A criterion was derived for the left hand side of the FLD based on Hill's localized necking theory. For determination of the forming limits on the right hand side of the FLD, the M-K theory was used. Furthermore, on two- and three-ply stainless steel-clad aluminum sheets, punch-stretching tests were done. Jalali et al. [7, 8] investigated the formability of Al1100-St12 two-layer sheet analytically and experimentally. They showed that the FLD of two-layer sheet lies between those of elements which compose it. They also studied the influences of material parameters on formability of two-layer metallic sheet.

In this work, the formability of Al3105-St14 two-layer sheet is studied through analytical, experimental and numerical approaches. An analytical model is presented based on Marciniak-Kuczynski method using Hill's non-quadratic yield criterion. Forming limit diagrams are also obtained numerically based on finite element method using Bifurcation theory and ductile fracture criteria. Analytical and numerical results are compared with experimental ones to examine the validity of theoretical approaches.

## 2. Theoretical Analysis

The Marciniak - Kuczynski [9] (M-K) forming limit model is extended in order to predict localized necking in sheet metal forming. Main assumption in this theory is considering a local heterogeneity in the sheet which is an initial imperfection in the form of a groove related to surface roughness [10] perpendicular to greater principal stress direction. Thus, there are two homogenous and inhomogeneous regions that are nominated as "a" and "b", respectively. As shown in Fig. 1, this groove is assumed to be perpendicular to maximum principal stress on material surface. The plane stress condition is considered. The sheet is stretched under biaxial tension by principal stresses  $\sigma_1$  and  $\sigma_2$ . The rolling directions of layers are coincident and assumed as principle direction.

The imperfection factor  $f$  is determined as the thickness ratio:

$$f = \frac{\sum t^{b(i)}}{\sum t^{a(i)}} \quad (1)$$

In which  $t^{a(i)}$  and  $t^{b(i)}$  are the thicknesses of homogenous and heterogeneous regions of layers, respectively. During the forming process, thicknesses of each layer in the homogenous and heterogeneous regions change in comparison with initial ones. The thickness of the homogenous region is:

$$t^{a(i)} = t_0^{a(i)} \cdot \exp(\varepsilon_3^{a(i)}) \quad (2)$$

In which  $t_0^{a(i)}$  and  $t^{a(i)}$  are initial and current thickness of  $i^{th}$  layer in homogenous region, respectively and  $\varepsilon_3^{a(i)}$  is the thickness strain.

Considering the initial value of the coefficient of heterogeneity is described by initial surface roughness and grain size [10, 11, 12], the imperfection factor can be expressed as:

$$f = \frac{t_0^{a(i)} - 2(R_G^{(i)} + k^{(i)}d_0^{(i)}\bar{\varepsilon}^{b(i)})}{t_0^{a(i)}} \exp(\varepsilon_3^{b(i)} - \varepsilon_3^{a(i)}) \quad (3)$$

Where  $R_G^{(i)}$  is the initial surface roughness,  $k^{(i)}$  is the coefficient of grain size,  $d_0^{(i)}$  is the grain size,  $\bar{\varepsilon}^{b(i)}$  is the effective strain in the heterogeneous region,  $\varepsilon_3^{a(i)}$  and  $\varepsilon_3^{b(i)}$  are the thickness strains of the homogeneous and heterogeneous regions for layer  $i$ , respectively.

Hill's non-quadratic yield criterion [13] is expressed as:

$$j|\sigma_2 - \sigma_1|^M + g|\sigma_3 - \sigma_1|^M + h|\sigma_1 - \sigma_2|^M + p|2\sigma_1 - \sigma_2 - \sigma_3|^M + q|2\sigma_2 - \sigma_1 - \sigma_3|^M + l|2\sigma_3 - \sigma_1 - \sigma_2|^M = \bar{\sigma}^M \quad (4)$$

In which the exponent  $M$  depends on material.  $j$ ,  $g$ ,  $h$ ,  $p$ ,  $q$  and  $l$  are anisotropy parameters. The yield function, under the plane stress condition and in-plane isotropy, is written as follows:

$$|\sigma_1 + \sigma_2|^M + (2r + 1)|\sigma_1 - \sigma_2|^M = 2(r + 1)\bar{\sigma}^M \quad (5)$$

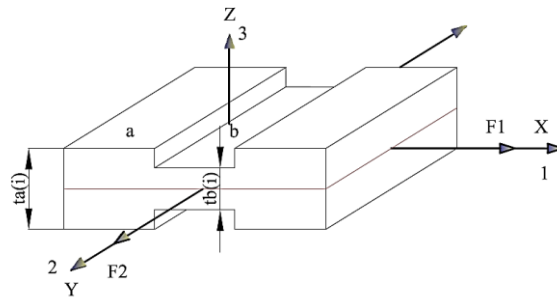


Fig. 1. Model of localized necking for two-layer sheet.

The stress ratio ( $\alpha$ ) and strain ratio ( $\rho$ ) are defined as:

$$\rho = \frac{d\varepsilon_2}{d\varepsilon_1} \tag{6}$$

$$\alpha = \frac{\sigma_2}{\sigma_1} \tag{7}$$

The associated flow rule is taken to be:

$$d\varepsilon_{ij} = d\lambda \frac{\partial Q}{\partial \sigma_{ij}} \tag{8}$$

where  $d\lambda$  is the proportionality factor and  $Q$  is the plastic potential defined by the yield function. Flow rule associated with Hill's yield criterion can be written as:

$$\begin{aligned} \frac{d\varepsilon_1}{|\sigma_1 + \sigma_2|^{M-1} + (1 + 2r)|\sigma_1 - \sigma_2|^{M-1}} &= \frac{d\varepsilon_2}{|\sigma_1 + \sigma_2|^{M-1} - (1 + 2r)|\sigma_1 - \sigma_2|^{M-1}} \\ &= \frac{-d\varepsilon_3}{d\bar{\varepsilon}} = \frac{2(1+r)\bar{\sigma}^{M-1}}{2|\sigma_1 + \sigma_2|^{M-1}} \end{aligned} \tag{9}$$

Accordingly

$$\rho = \frac{|1 + \alpha|^{M-1} - (1 + 2r)|1 - \alpha|^{M-1}}{|1 + \alpha|^{M-1} + (1 + 2r)|1 - \alpha|^{M-1}} \tag{10}$$

According to equilibrium condition, the forces acting on the homogenous and heterogeneous regions are equal:

$$\sum_{i=1}^2 F_1^{a(i)} = \sum_{i=1}^2 F_1^{b(i)} \tag{11}$$

In which  $F_1^{a(i)}$  and  $F_1^{b(i)}$  are forces applied on direction 1 in regions "a" and "b" for  $i^{th}$  layer.

Considering isotropic work hardening and strain rate hardening, the behavior of the material for each layer can be expressed as:

$$\bar{\sigma}^{(i)} = C^{(i)}(\bar{\varepsilon}^{(i)})^{n^{(i)}}(\dot{\bar{\varepsilon}}^{(i)})^{m^{(i)}} \tag{12}$$

Where  $C^{(i)}$  is the strength coefficient,  $n^{(i)}$  is strain hardening exponent and  $m^{(i)}$  is strain sensitivity coefficient for  $i^{th}$  layer.

By defining the dimensionless parameter  $\varphi$  as:

$$\varphi = \frac{\sigma_1}{\bar{\sigma}} = \frac{2(1+r)}{|1 + \alpha|^M + (1 + 2r)|1 - \alpha|^M} \tag{13}$$

The equilibrium equation can be written as:

$$\sum_{i=1}^2 \varphi^{a(i)} (\bar{\varepsilon}^{a(i)})^{n(i)} (\dot{\bar{\varepsilon}}^{a(i)})^{m(i)} \cdot t^{a(i)} = \sum_{i=1}^2 \varphi^{b(i)} (\bar{\varepsilon}^{b(i)})^{n(i)} (\dot{\bar{\varepsilon}}^{b(i)})^{m(i)} \cdot t^{b(i)} \quad (14)$$

The Compatibility requirement between the regions “a” and “b” yields to equality of strains at direction 2 of two regions for each layer:

$$d\varepsilon_2^{b(i)} = d\varepsilon_2^{a(i)} \quad (15)$$

Combining equations (5), (9), (13) and (15) gives the effective strain increment in the heterogeneous region as:

$$d\bar{\varepsilon}^b = \frac{2(1+r)d\varepsilon_2^a}{|1 + \alpha^b|^{(M-1)} - (1+2r)|1 - \alpha^b|^{(M-1)}} \left[ \frac{|1 + \alpha^b|^M + (1+2r)|1 - \alpha^b|^M}{2(1+r)} \right]^{(M-1)/M} \quad (16)$$

The relation between effective strain increment and principal strain increments is as follows [14, 15]:

$$d\bar{\varepsilon} = \frac{[2(1+r)]^{1/M}}{2} \left[ \frac{1}{(1+2r)^{1/(M-1)}} |d\varepsilon_1 - d\varepsilon_2|^{M/(M-1)} + |d\varepsilon_1 + d\varepsilon_2|^{M/(M-1)} \right]^{(M-1)/M} \quad (17)$$

The ratio of effective strain increment to strain increment in direction 1 can be obtained as:

$$\beta = \frac{d\bar{\varepsilon}}{d\varepsilon_1} = \frac{[2(1+r)]^{1/M}}{2} \left[ \frac{1}{(1+2r)^{1/(M-1)}} |1 - \rho|^{M/(M-1)} + |1 + \rho|^{M/(M-1)} \right]^{(M-1)/M} \quad (18)$$

The limit strains are determined by solving above mentioned equations numerically, using following algorithm:

1) Considering a loading path, a finite increment of principal strain ( $d\varepsilon_1$ ) is imposed on the homogenous regions for two layers.  $\alpha$ ,  $\beta$ ,  $\varphi$ , other principal strain increments ( $d\varepsilon_2, d\varepsilon_3$ ), effective strain increment ( $d\bar{\varepsilon}$ ) and effective stress ( $\bar{\sigma}$ ) of mentioned region are calculated for each layer using equations (9), (10), (13) and (18).

2) Regarding no slippery condition between layers throughout forming process ( $\rho_{layer1} = \rho_{layer2}$ ), based on equilibrium condition, equations (14), the stress ratios in heterogeneous regions for two layers ( $\alpha^{b(1)}, \alpha^{b(2)}$ ) can be calculated.

3) Knowing  $\alpha^{b(1)}, \alpha^{b(2)}$  for two layers,  $\rho$ ,  $\beta$  and  $\varphi$  in heterogeneous region can be determined using equations (10), (13) and (18). So, the strain increments and stress components of two layers are obtained in this zone. If the ratio  $\frac{d\bar{\varepsilon}^{b(i)}}{d\varepsilon^{a(i)}}$  for one of layers becomes greater than 10, the current values of  $\varepsilon_2^{a(i)}, \varepsilon_1^{a(i)}$  can specify a point of FLD.

4) If the above mentioned ratio isn't greater than 10, the calculation route will be repeated with adding a strain increment  $d\varepsilon_1$  to the previous amount of strain.

5) Computation will be conducted while  $\rho$  is from -0.5 to 1.0.

### 3. Experimental Procedure

In order to determine the forming limits of two-layer sheets in experimental study, the Hecker out of plane stretching test [16] was used. Two-layer sheets consist of 0.5 mm thickness aluminum Al3105 sheet and 0.5 mm thickness carbon steel St14 sheet were used.

Material properties of each layer are listed in Table 1. The adhesive that joined layers together was Polyurethane. Figure 2 and Table 2 show the dimensions of specimens. Experimental set up is shown in Fig. 3. The ram speed was 5 mm/min throughout doing experimental tests. The steel side of specimens was

contacted with hemispherical punch. Circular grids of 5 mm diameter were printed on surfaces of the specimens to measure the strains experimentally. The major and minor strains of localized necking region were calculated with geometry of the deformed grids as follow:

$$\varepsilon_1 = \ln \frac{D_1}{D_0} \tag{19}$$

$$\varepsilon_2 = \ln \frac{D_2}{D_0} \tag{20}$$

where  $\varepsilon_1$  is major strain and  $\varepsilon_2$  is minor strain.  $D_0$  is initial diameter of grids and  $D_1$  and  $D_2$  are major and minor diameters of deformed grids, respectively. Figure 4 shows 75 × 200 mm specimen after forming.

Table 1. Material properties Al3105 and St14 sheets.

Variables	Values	
Material	St14	Al 3105
Thickness, $t$ (mm)	0.5	0.5
Young's modulus, $E$ (GPa)	210	70
Poisson's ratio	0.3	0.33
Density, (Kg/m <sup>3</sup> )	7850	2700
Strength coefficient, $C$ (MPa)	548.44	302
Strain hardening exponent, $n$	0.229	0.103
Strain rate sensitivity exponent, $m$	0.01	0.001
Surface Roughness, $R_0$ ( $\mu m$ )	4	1.6
Anisotropy parameter, $r_0$	1.77	0.2
Anisotropy parameter, $r_{90}$	1.95	0.24
Grain size, $d_0$ ( $\mu m$ )	10	20

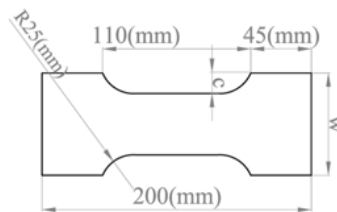


Fig. 2. Schematic of the specimens.

Table 2. The dimensions of specimens.

No.	1	2	3	4	5	6	7	8
W(mm)	75	100	125	150	125	150	175	200
C(mm)	17.5	25	25	25	-	-	-	-



Fig. 3. Experimental set-up.



Fig. 4. The 75 mm×200 mm specimen after forming.

#### 4. Numerical Study

In order to do the numerical study of the formability of two-layer metallic sheets, all the consumed geometries in experimental study were simulated using commercially available finite element code ABAQUS/ Standard. In other word, experimental conditions were duplicated in numerical simulation. Punch, die and blank holder were rigid bodies, while two-layer metallic sheets were deformable. Sheets were modeled using four-node shell elements S4R with two integrations. One-quarter of the geometry was modeled due to symmetry condition. A default surface to surface contact explicit used to specify the interfaces between the surfaces of the tooling and the blank. The tie constraint was used between two layers by assuming there is no slipping among layers.

The used surface to surface contact algorithm was automatic to define the interfaces between the surfaces of the tooling and the sheet. This algorithm is based on the penalty method. Coulomb friction model with a constant friction coefficient of 0.1 was used between the sheet-die and sheet-blank holder interface. A friction coefficient of 0.3 was assumed between the blank and the punch. The simulations were performed for 8 specimens given in Fig. 2 to determine the FLD numerically. Figure 5 shows simulated 75mm × 200mm specimen. Two different criteria were employed to predict the onset of failure in numerical study:

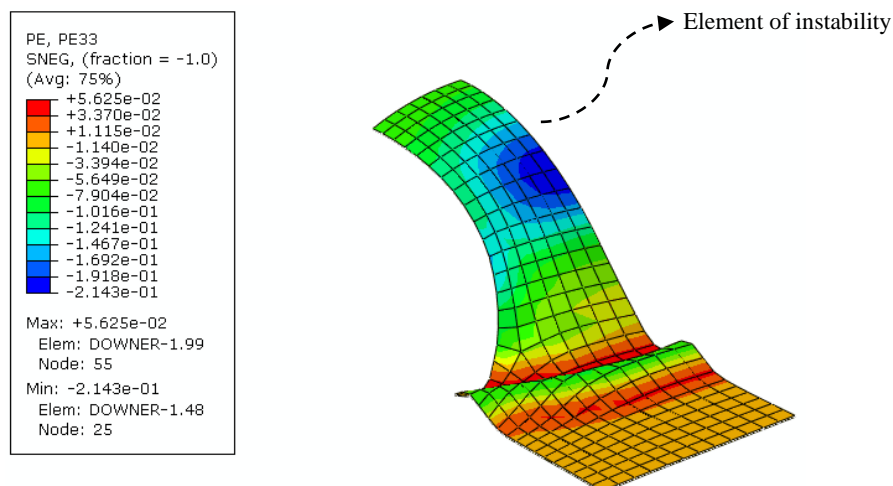


Fig. 5. Formed 75 mm × 200 mm Specimen in numerical simulation.

##### 4.1. Bifurcation criterion

Sheet metal formability is often limited by the onset of localized necking. A numerical method to access the forming limit diagram is bifurcation theory. In bifurcation theory [17, 18, 19], onset of necking can be seen

in diagram of second differentiate of thickness with respect to time and the abrupt changing of thickness strain.

The variation of thickness strain of 75mm×200mm sample with respect to time can be seen in Fig. 6a.

The second differentiate of thickness strain respect to time for the 75mm × 200mm specimen is illustrated in Fig. 6b. The minimum point represents occurrence of necking.

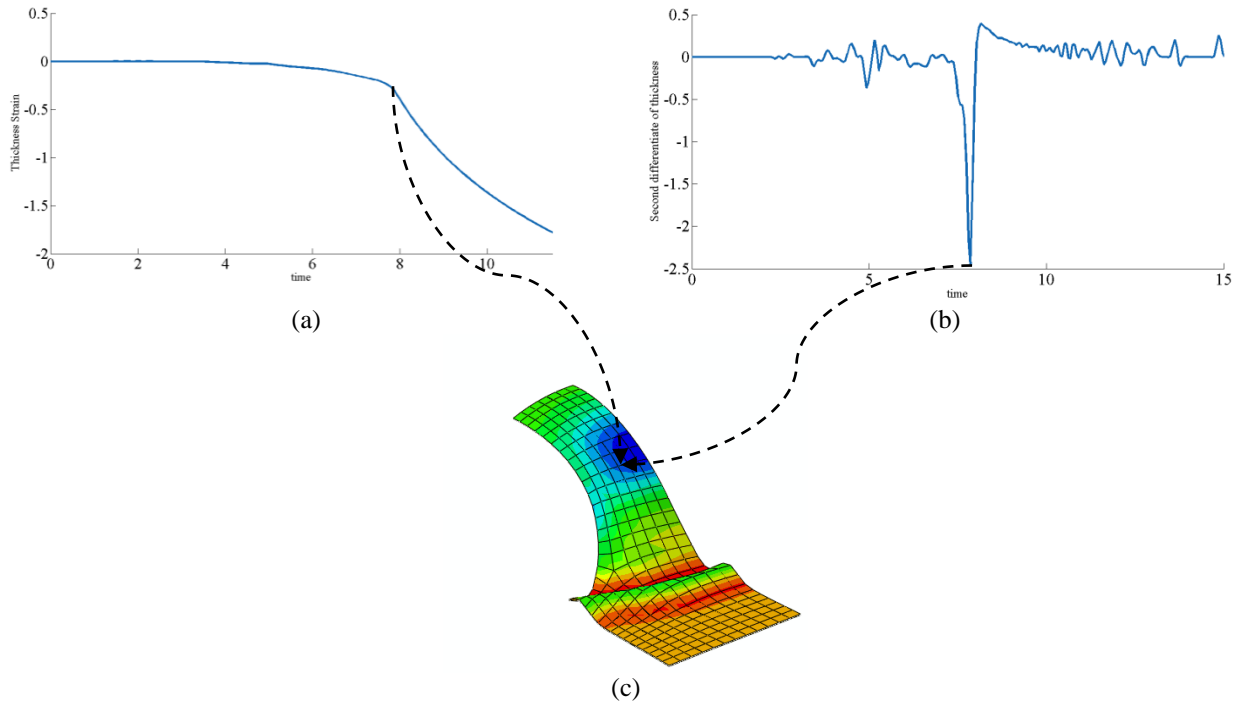


Fig. 6. (a) Thickness strain and (b) second differentiate of thickness strain versus time for 75 mm × 200 mm Specimen (c) Formed 75 mm × 200 mm Specimen

#### 4.2. Ductile fracture criteria

Deformation history considered in many of ductile fracture criteria affects formability of sheet metals. Thus, ductile fracture criteria can be employed as a potent tool to predict the forming limits of sheet metals. In the following, two ductile fracture criteria used in this work will be explained.

Cockroft and Lathman [20] proposed a criterion considering the role of the largest tensile stress in initiation of fracture. Oh et al. [21] modified the Cockroft and Latham criterion and suggest a criterion as follows:

$$\int_0^{\bar{\epsilon}_f} \frac{\sigma_1}{\bar{\sigma}} d\bar{\epsilon} = C_1 \tag{21}$$

where,  $\sigma_1$  is the maximum principal stress,  $\bar{\sigma}$  is the effective stress and  $C_1$  is material constant.

Brozzo et al. [22] presented a criterion in which the influences of the largest principal stress and the hydrostatic stress on initiation of fracture were considered:

$$\int_0^{\bar{\epsilon}_f} \frac{2\sigma_1}{3(\sigma_1 - \sigma_m)} d\bar{\epsilon} = C_2 \tag{22}$$

In which,  $\sigma_m$  is the hydrostatic stress and  $C_2$  is the material constant.

In order to determine the material constants in Oh and Brozzo ductile fracture criteria, uniaxial tension tests were done for each material. Knowing fracture strain from uniaxial tension test, the material constants for each material were calculated using equations of criteria regarding stress state of uniaxial tension.

The calculated material constants  $C_1$  and  $C_2$  for Al3105 and St14 sheets are listed in Table 3.

Table 3. The calculated material constants  $C_1$  and  $C_2$  for Al3105 and St14 sheets

Material	$C_1$	$C_2$
Al3105	0.12	0.1
St14	0.27	0.26

**5. Result and Discussion**

Figure 7 shows the forming limit diagram of Al3105-St14 two-layer sheet compared with those of its components obtained experimentally. It can be seen that FLD of two-layer sheet is located between the FLDs of elements which compose it. Mechanical and geometrical properties of layers determine the exact location of the FLD of the two-layer sheet.

The analytical FLDs of Al3105-St14 two-layer sheet and its components calculated based on M-K method using Hill’s non-quadratic yield criterion are depicted in Fig. 8.

Moreover, Fig. 9 represents numerical FLDs of Al3105-St14 two-layer sheet and separate layers based on Oh and Brozzo ductile fracture criteria.

Analytical, Numerical and experimental results demonstrate that the formability of two-layer sheet is better than the component with lower formability.

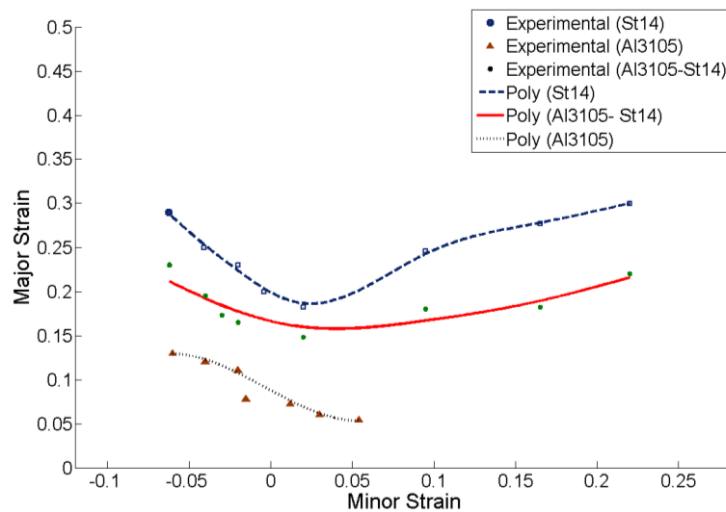


Fig. 7. Experimental FLDs of Al3105-St14 two-layer sheet and its components.

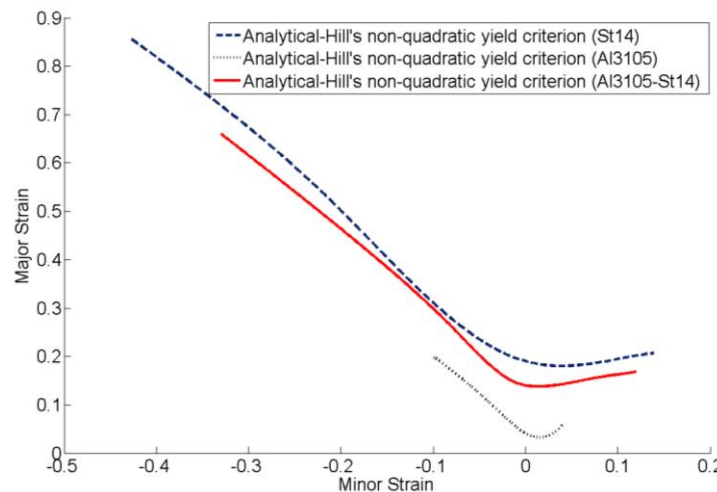


Fig. 8. FLDs of Al3105-St14 two-layer sheet and its components obtained from analytical model.



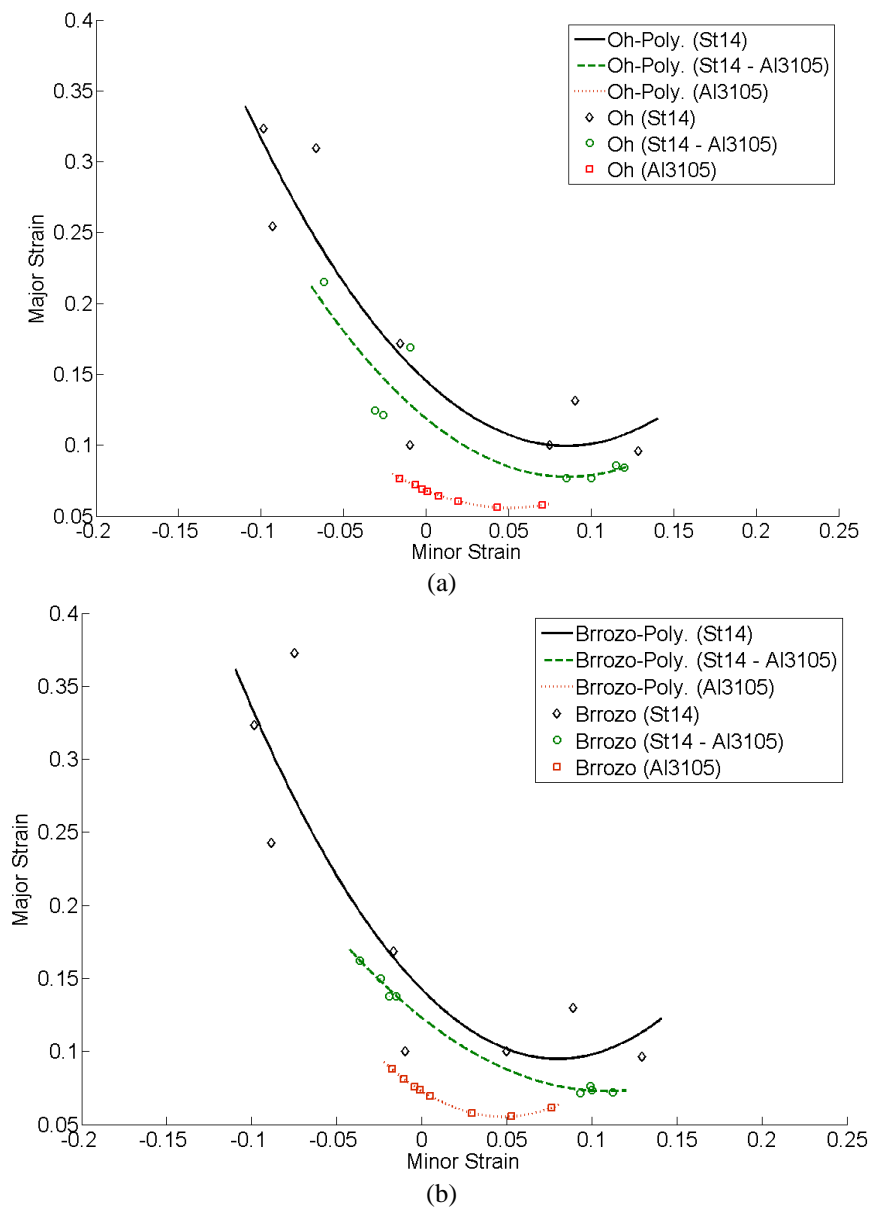


Fig. 9. Numerical FLDs of Al3105-St14 two-layer sheet and its components based on a) Oh and b) Brozzo ductile fracture criteria.

Forming limit diagram analytically obtained from M-K model associated Hill's non-quadratic yield criterion, FLDs determined numerically based on Oh and Brozzo ductile fracture criteria, numerically predicted FLD using bifurcation theory and experimental results for Al3105-St14 two-layer sheet are compared and the result is shown in Fig. 10.

It is seen that FLDs calculated from analytical and numerical methods are in a good agreement with experimental results. Hence, it can be concluded that the above-mentioned analytical and numerical approaches have good capabilities to predict the formability of two-layer sheets. However, the FLD obtained analytically by M-K theory and the FLD predicted numerically based on bifurcation theory are more compatible with experiments. It shows that these methods are more suitable to predict forming limits of carbon steel St14 and aluminum alloy Al3105 two-layer sheets.

In Fig. 11 the influence of thickness ratio of layers on formability of Al3105-St14 two-layer sheet has been illustrated in the case of constancy of total thickness. The results demonstrate that increasing the thickness ratio ( $t_{St}/t_{Al}$ ) increases the formability of two-layer sheet.

As discussed, the FLD of two-layer sheet is located between the FLDs of separated layers. (Fig. 11) shows that the exact location of the FLD is affected by thickness ratio of layers.

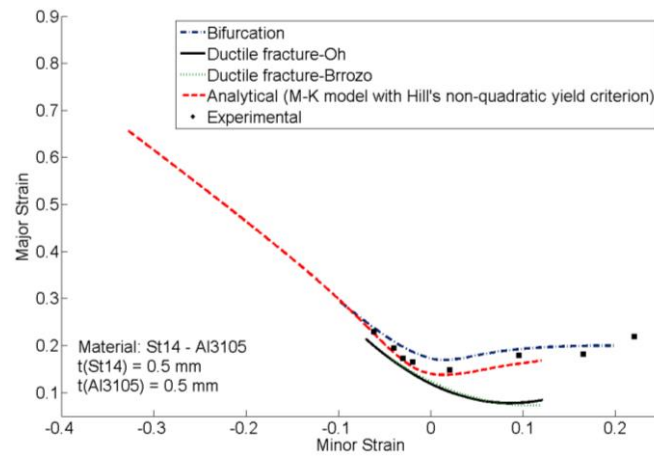


Fig. 10. Comparison between theoretical FLDs determined by various methods and experiments for Al3105-St14 two-layer sheet.

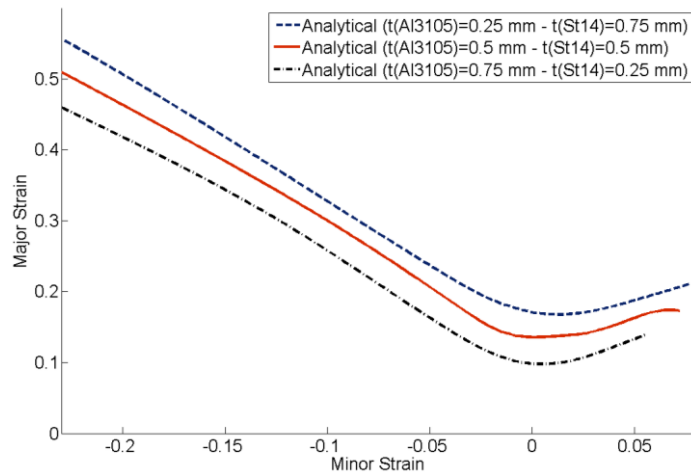


Fig. 11. The effect of the thickness ratio of layers on the FLD of Al3105-St14 two-layer sheet.

## 6. Conclusion

In this paper, an analytical model was developed to calculate the forming limits of two-layer sheet based on Marciniak-Kuczynski method using Hill's non-quadratic yield criterion. Bifurcation and ductile fracture criteria are also employed to determine the forming limit diagram of two-layer sheet numerically. Experiments were also carried out on Al3105-St14 two-layer sheet. The validity of the analytical and numerical results was examined by comparison with experimental ones. It can be concluded that:

- The forming limit diagram of two-layer sheet is located between FLDs of separate layers. It means that, the formability of two-layer sheet is better than the formability of layer with lower formability.
- Forming limits obtained from analytical and numerical methods were in a good agreement with experimental results. Hence, analytical and numerical approaches discussed in this paper have good capabilities to predict the formability of two-layer sheets. However, the analytical method based on M-K model and numerical approach based on bifurcation theory are more suitable to determine the forming limit diagram of carbon steel St14 and aluminum alloy Al3105 two-layer sheets, especially for the right hand side of the FLD.

- In the case of constancy of total thickness of two-layer sheet, increasing the thickness ratio ( $t_{St}/t_{Al}$ ) increases the formability.
- The exact location of the FLD of two-layer sheet is influenced by thickness ratio of layers.

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## مطالعه مقایسه‌ای پیش‌بینی شکل‌پذیری ورق‌های فلزی دو لایه حامد دیلمی عضدی\* و رویا دارابی

دانشکده مهندسی مکانیک، دانشگاه صنعتی اراک، اراک، ایران، کد پستی 38181-41167

**چکیده:** ورق‌های دولایه فلزی دارای کاربردهای فراوان در صنایع هوافضا، دریایی، خودرو و همچنین صنایع خانگی می‌باشند. در این مقاله، شکل‌پذیری ورق‌های دولایه فلزی به صورت تحلیلی، عددی و تجربی مورد بررسی قرار می‌گیرد. مدلی تحلیلی بر اساس روش مارسینیاک و کوزینسکی و با کمک معیار تسلیم غیر درجه 2 هیل ارائه شده است. همچنین، منحنی‌های حد شکل‌دهی به روش اجزاء محدود بر اساس تئوری‌های دو شاخه شدن (بایفورکیشن) و شکست نرم استخراج شده است. علاوه بر این، آزمایش‌های تجربی بر روی ورق دولایه Al3105-St14 انجام گرفته است. نتایج تئوری به دست آمده از روش‌های مختلف با هدف ارزیابی توانایی روش‌های عددی و تحلیلی مورد بررسی در پیش‌بینی شکل‌پذیری ورق‌های دولایه، با نتایج حاصل از آزمایش‌های تجربی مقایسه گردیده است. نتایج نشان می‌دهد، روش‌های عددی و تحلیلی مورد بررسی در این مقاله، دارای قابلیت مناسبی جهت پیش‌بینی شکل‌پذیری ورق‌های دولایه بود؛ ولیکن، روش تحلیلی مبتنی بر مدل مارسینیاک و کوزینسکی و روش عددی بر اساس تئوری دو شاخه شدن، جهت تعیین منحنی حد شکل‌دهی ورق‌های دولایه Al3105-St14 مناسب‌تر می‌باشند.

**واژه‌های کلیدی:** منحنی حد شکل‌دهی (FLD)، ورق دو لایه، مدل مارسینیاک و کوزینسکی (M-K)، معیار تسلیم غیر درجه 2 هیل، تئوری دو شاخه شدن (بایفورکیشن)، شکست نرم.